Chapter 9

9–14 An air-standard cycle with variable specific heats is executed in a closed system and is composed of the following four processes:

1-2 Isentropic compression from 100 kPa and 27°C to 800 kPa

2-3 \( v = \text{constant} \) heat addition to 1800 K

3-4 Isentropic expansion to 100 kPa

4-1 \( P = \text{constant} \) heat rejection to initial state

(a) Show the cycle on \( P-v \) and \( T-s \) diagrams.

(b) Calculate the net work output per unit mass.

(c) Determine the thermal efficiency.

9-14 The four processes of an air-standard cycle are described. The cycle is to be shown on \( P-v \) and \( T-s \) diagrams, and the net work output and the thermal efficiency are to be determined.

**Assumptions**

1. The air-standard assumptions are applicable.
2. Kinetic and potential energy changes are negligible.
3. Air is an ideal gas with variable specific heats.

**Properties**
The properties of air are given in Table A-17.

**Analysis**

(b) The properties of air at various states are

\[
T_1 = 300 K \quad h_1 = 300.19 \text{ kJ/kg}
\]

\[
P_{r_1} = 1.386
\]

\[
P_{r_2} = \frac{P_2}{P_1} = \frac{800 \text{ kPa}}{100 \text{ kPa}} = 8 \Rightarrow u_2 = \frac{800 kPa}{100 kPa} \Rightarrow T_2 = 539.8 K
\]

\[
T_3 = 1800 K \quad u_3 = 1487.2 \text{ kJ/kg}
\]

\[
T_4 = 539.8 K
\]

\[
P_{r_3} = \frac{P_3}{P_2} = \frac{100 \text{ kPa}}{2668 \text{ kPa}} \Rightarrow P_{r_3} = 1310
\]

\[
P_{r_4} = \frac{P_4}{P_3} = \frac{100 \text{ kPa}}{2668 \text{ kPa}} \Rightarrow 49.10 \Rightarrow h_4 = 828.1 \text{ kJ/kg}
\]

From energy balances,

\[
q_{in} = u_3 - u_2 = 1487.2 - 389.2 = 1098.0 \text{ kJ/kg}
\]

\[
q_{out} = h_4 - h_1 = 828.1 - 300.19 = 527.9 \text{ kJ/kg}
\]

\[
w_{net,out} = q_{in} - q_{out} = 1098.0 - 527.9 = 570.1 \text{ kJ/kg}
\]

(c) Then the thermal efficiency becomes

\[
\eta_{th} = \frac{w_{net,out}}{q_{in}} = \frac{570.1 \text{ kJ/kg}}{1098.0 \text{ kJ/kg}} = 51.9\%
\]
Consider a Carnot cycle executed in a closed system with 0.003 kg of air. The temperature limits of the cycle are 300 and 900 K, and the minimum and maximum pressures that occur during the cycle are 20 and 2000 kPa. Assuming constant specific heats, determine the net work output per cycle.

A Carnot cycle with the specified temperature limits is considered. The net work output per cycle is to be determined.

**Assumptions** Air is an ideal gas with constant specific heats.

**Properties** The properties of air at room temperature are $c_p = 1.005 \text{ kJ/kg·K}$, $c_v = 0.718 \text{ kJ/kg·K}$, $R = 0.287 \text{ kJ/kg·K}$, and $k = 1.4$ (Table A-2).

**Analysis** The minimum pressure in the cycle is $P_3$ and the maximum pressure is $P_1$. Then,

$$\frac{T_2}{T_3} = \left(\frac{P_2}{P_3}\right)^{\frac{k-1}{k}}$$

or,

$$P_2 = P_3 \left(\frac{T_2}{T_3}\right)^{\frac{k}{k-1}} = (20 \text{ kPa}) \left(\frac{900 \text{ K}}{300 \text{ K}}\right)^{\frac{1.4}{0.4}} = 935.3 \text{ kPa}$$

The heat input is determined from

$$s_2 - s_1 = c_p \ln \frac{T_2}{T_1} - R \ln \frac{P_2}{P_1} = -(0.287 \text{ kJ/kg·K}) \ln \frac{935.3 \text{ kPa}}{2000 \text{ kPa}} = 0.2181 \text{ kJ/kg·K}$$

$$Q_{in} = mT_H(s_2 - s_1) = (0.003 \text{ kg})(900 \text{ K})(0.2181 \text{ kJ/kg·K}) = 0.5889 \text{ kJ}$$

Then,

$$\eta_{th} = 1 - \frac{T_4}{T_H} = 1 - \frac{300 \text{ K}}{900 \text{ K}} = 66.7\%$$

$$W_{net,out} = \eta_{th} Q_{in} = (0.667)(0.5889 \text{ kJ}) = 0.393 \text{ kJ}$$
An ideal Otto cycle has a compression ratio of 8. At the beginning of the compression process, air is at 95 kPa and 27°C, and 750 kJ/kg of heat is transferred to air during the constant-volume heat-addition process. Taking into account the variation of specific heats with temperature, determine (a) the pressure and temperature at the end of the heat addition process, (b) the net work output, (c) the thermal efficiency, and (d) the mean effective pressure for the cycle. Answers: (a) 3898 kPa, 1539 K, (b) 392.4 kJ/kg, (c) 52.3 percent, (d) 495 kPa

An ideal Otto cycle with air as the working fluid has a compression ratio of 8. The pressure and temperature at the end of the heat addition process, the net work output, the thermal efficiency, and the mean effective pressure for the cycle are to be determined.

Assumptions

1. The air-standard assumptions are applicable.
2. Kinetic and potential energy changes are negligible.
3. Air is an ideal gas with variable specific heats.

Properties

The gas constant of air is \( R = 0.287 \text{ kJ/kg.K} \). The properties of air are given in Table A-17.

Analysis

(a) Process 1-2: isentropic compression.

\[
T_1 = 300 \text{K} \quad \Rightarrow \quad u_1 = 214.07 \text{kJ/kg} \quad \nu_1 = 621.2
\]

\[
\nu_2 = \frac{\nu_2}{\nu_1} \quad \nu_1 = \frac{1}{r} \quad \nu_1 = \frac{1}{8} (621.2) = 77.65 \quad \Rightarrow \quad T_2 = 673.1 \text{K} \quad u_2 = 491.2 \text{ kJ/kg}
\]

\[
\frac{P_2 \nu_2}{T_2} = \frac{P_1 \nu_1}{T_1} \quad \Rightarrow \quad P_2 = \frac{\nu_2}{\nu_1} \quad T_2 = (8) \left( \frac{673.1 \text{ K}}{300 \text{ K}} \right) (95 \text{ kPa}) = 1705 \text{ kPa}
\]

Process 2-3: \( \nu \) = constant heat addition.

\[
q_{23,\text{in}} = u_3 - u_2 \quad \Rightarrow \quad u_3 = u_2 + q_{23,\text{in}} = 491.2 + 750 = 1241.2 \text{ kJ/kg} \quad \Rightarrow \quad u_3 = 1539 \text{ K} \quad \nu_3 = 6.588
\]

\[
\frac{P_3 \nu_3}{T_3} = \frac{P_2 \nu_2}{T_2} \quad \Rightarrow \quad P_3 = \frac{T_3}{T_2} \quad P_3 = \left( \frac{1539 \text{ K}}{673.1 \text{ K}} \right) (1705 \text{ kPa}) = 3898 \text{ kPa}
\]

(b) Process 3-4: isentropic expansion.

\[
\nu_4 = \frac{\nu_4}{\nu_3} = r \nu_3 = (8)(6.588) = 52.70 \quad \Rightarrow \quad T_4 = 774.5 \text{ K} \quad u_4 = 571.69 \text{ kJ/kg}
\]

Process 4-1: \( \nu \) = constant heat rejection.

\[
q_{\text{out}} = u_4 - u_1 = 571.69 - 214.07 = 357.62 \text{ kJ/kg}
\]

\[
w_{\text{net, out}} = q_{\text{in}} - q_{\text{out}} = 750 - 357.62 = 392.4 \text{ kJ/kg}
\]
An air-standard Diesel cycle has a compression ratio of 16 and a cutoff ratio of 2.

At the beginning of the compression process, air is at 95 kPa and 27°C. Accounting for the variation of specific heats with temperature, determine (a) the temperature after the heat-addition process, (b) the thermal efficiency, and (c) the mean effective pressure.

**Answers:** (a) 1724.8 K, (b) 56.3 percent, (c) 675.9 kPa

An air-standard Diesel cycle with a compression ratio of 16 and a cutoff ratio of 2 is considered. The temperature after the heat addition process, the thermal efficiency, and the mean effective pressure are to be determined.

**Assumptions**

1. The air-standard assumptions are applicable.
2. Kinetic and potential energy changes are negligible.
3. Air is an ideal gas with variable specific heats.

**Properties**

The gas constant of air is \( R = 0.287 \text{ kJ/kg.K} \). The properties of air are given in Table A-17.

**Analysis**

(a) Process 1-2: isentropic compression.

\[
\frac{T_1}{T_2} = \frac{R}{P_1} \rightarrow \frac{u_1}{u_2} = \frac{v_2}{v_1} = \frac{v_3}{v_4} = \frac{1}{r} = \frac{1}{16} = 0.0625
\]

\[
\frac{q_{in}}{q_{out}} = \frac{v_3}{v_2} = \frac{T_3}{T_2} = \frac{v_2}{v_1} = \frac{v_3}{v_4} = \frac{1}{r} = \frac{1}{16} = 0.0625
\]

(b) \( q_{in} = h_3 - h_2 = 1910.6 - 890.9 = 1019.7 \text{ kJ/kg} \)

Process 3-4: isentropic expansion.

\[
\frac{v_3}{v_2} = \frac{v_4}{v_1} = \frac{r}{2} = \frac{16}{2} = 8 \rightarrow u_4 = 659.7 \text{ kJ/kg}
\]
$$q_{\text{out}} = u_4 - u_1 = 659.7 - 214.07 = 445.63 \text{ kJ/kg}$$

$$\eta_{\text{th}} = 1 - \frac{q_{\text{out}}}{q_{\text{in}}} = 1 - \frac{445.63 \text{ kJ/kg}}{1019.7 \text{ kJ/kg}} = 56.3\%$$

(c) $$w_{\text{net}, \text{out}} = q_{\text{in}} - q_{\text{out}} = 1019.7 - 445.63 = 574.07 \text{ kJ/kg}$$

$$\nu_1 = \frac{RT_1}{P_1} = \frac{(0.287 \text{ kPa} \cdot \text{m}^3/\text{kg} \cdot \text{K}) \cdot (300 \text{ K})}{95 \text{ kPa}} = 0.906 \text{ m}^3/\text{kg} = \nu_{\text{max}}$$

$$\nu_{\text{min}} = \nu_2 = \frac{\nu_{\text{max}}}{r}$$

$$\text{MEP} = \frac{w_{\text{net}, \text{out}}}{\nu_1 - \nu_2} = \frac{w_{\text{net}, \text{out}}}{\nu_1 (1 - 1/r)} = \frac{574.07 \text{ kJ/kg}}{(0.906 \text{ m}^3/\text{kg} \cdot (1 - 1/16))(\text{kJ/kg} \cdot \text{m}^3/\text{K})} = 675.9 \text{ kPa}$$

9-84 A gas-turbine power plant operates on the simple Brayton cycle between the pressure limits of 100 and 1200 kPa. The working fluid is air, which enters the compressor at 30°C at a rate of 150 m3/min and leaves the turbine at 500°C. Using variable specific heats for air and assuming a compressor isentropic efficiency of 82 percent and a turbine isentropic efficiency of 88 percent, determine (a) the net power output, (b) the back work ratio, and (c) the thermal efficiency. **Answers:** (a) 659 kW, (b) 0.625, (c) 0.319

9-84 A gas-turbine plant operates on the simple Brayton cycle. The net power output, the back work ratio, and the thermal efficiency are to be determined.

**Assumptions**

1. The air-standard assumptions are applicable.
2. Kinetic and potential energy changes are negligible.
3. Air is an ideal gas with variable specific heats.

**Properties**

The gas constant of air is $$R = 0.287 \text{ kJ/kg-K}$$ (Table A-1).

**Analysis**

(a) For this problem, we use the properties from EES software. Remember that for an ideal gas, enthalpy is a function of temperature only whereas entropy is functions of both temperature and pressure.

**Process 1-2:** Compression

$$T_1 = 30^\circ\text{C} \rightarrow h_1 = 303.60 \text{ kJ/kg}$$

$$T_1 = 30^\circ\text{C}$$

$$P_1 = 100 \text{ kPa}$$

$$s_2 = s_1 = 5.7159 \text{ kJ/kg-K}$$

$$P_2 = 1200 \text{ kPa}$$

$$h_2 = 617.37 \text{ kJ/kg}$$
\[ \eta_C = \frac{h_2 - h_i}{h_2 - h_i} \rightarrow 0.82 = \frac{617.37 - 303.60}{h_2 - 303.60} \rightarrow h_2 = 686.24 \text{ kJ/kg} \]

Process 3-4: Expansion

\[ T_4 = 500^\circ C \rightarrow h_4 = 792.62 \text{ kJ/kg} \]

\[ \eta_T = \frac{h_3 - h_4}{h_3 - h_4} \rightarrow 0.88 = \frac{h_3 - 792.62}{h_3 - h_4} \]

We cannot find the enthalpy at state 3 directly. However, using the following lines in EES together with the isentropic efficiency relation, we find \( h_3 = 1404.7 \text{ kJ/kg}, T_3 = 1034^\circ C, s_3 = 6.5699 \text{ kJ/kg.K} \). The solution by hand would require a trial-error approach.

\[ h_3 = \text{enthalpy(Air, } T=T_3) \]
\[ s_3 = \text{entropy(Air, } T=T_3, P=P_2) \]
\[ h_4 = \text{enthalpy(Air, } P=P_1, s=s_3) \]

The mass flow rate is determined from

\[ \dot{m} = \frac{P \dot{V}}{RT_1} = \frac{(100 \text{ kPa})(150/60 \text{ m}^3/\text{s})}{(0.287 \text{ kPa} \cdot \text{m}^3/\text{kg} \cdot \text{K})(30 + 273 \text{ K})} = 2.875 \text{ kg/s} \]

The net power output is

\[ W_{C,\text{in}} = \dot{m}(h_2 - h_1) = (2.875 \text{ kg/s})(686.24 - 303.60) \text{kJ/kg} = 1100 \text{ kW} \]
\[ W_{T,\text{out}} = \dot{m}(h_3 - h_4) = (2.875 \text{ kg/s})(1404.7 - 792.62) \text{kJ/kg} = 1759 \text{ kW} \]
\[ W_{\text{net}} = W_{T,\text{out}} - W_{C,\text{in}} = 1759 - 1100 = 659 \text{ kW} \]

(b) The back work ratio is

\[ r_{\text{bw}} = \frac{W_{C,\text{in}}}{W_{T,\text{out}}} = \frac{1100 \text{ kW}}{1759 \text{ kW}} = 0.625 \]

(c) The rate of heat input and the thermal efficiency are

\[ Q_{\text{in}} = \dot{m}(h_3 - h_2) = (2.875 \text{ kg/s})(1404.7 - 686.24) \text{kJ/kg} = 2065 \text{ kW} \]
\[ \eta_{th} = \frac{W_{\text{net}}}{Q_{\text{in}}} = \frac{659 \text{ kW}}{2065 \text{ kW}} = 0.319 \]