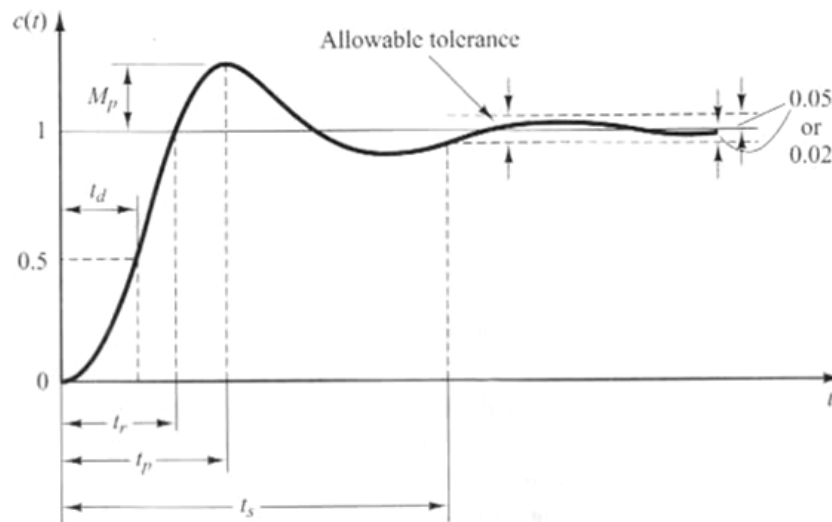


## Control System Design

**Performance Specifications:** Time domain and Frequency domain

- Absolute and Relative stability
- Speed of dynamic responses
- Accuracy at steady state operation

Unit-step response for input  $R(s) = \frac{1}{s}$



- Rise time ( $t_r$ ), Peak time ( $t_p$ ), Settling time ( $t_s$ ) 5% error or 2% error
- %Percent overshoot, Maximum overshoot ( $M_p$ )
- Steady state error for step input, Static position error constant ( $K_p$ )

Unit-ramp response for input  $R(s) = \frac{1}{s^2}$

- Steady state error for ramp input, Static velocity error constant, ( $K_v$ )

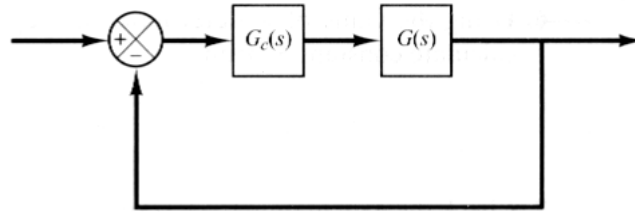
### Open-loop transfer function

- Type of system in unity feedback control system
- Gain margin(GM), (dB); Phase margin(PM), (degree), Damping ratio( $\zeta$ ),

### Closed-loop transfer function

- Natural frequency ( $\omega_n$ ), rad/sec; Damping ratio( $\zeta$ ), Gain
- Bandwidth frequency ( $\omega_{BW}$ ), rad/sec

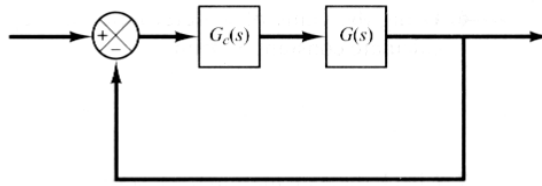
Control system diagram in unity feedback



$G_c(s)$  – Compensator / Controller;  $G(s)$  – Plant / Transfer function

Function	Compensator	Transfer function	Characteristics
Improve steady-state error	PI	$K \frac{s + z_c}{s}$	<ol style="list-style-type: none"> <li>Increases system type.</li> <li>Error becomes zero.</li> <li>Zero at <math>-z_c</math> is small and negative.</li> <li>Active circuits are required to implement.</li> </ol>
Improve steady-state error	Lag	$K \frac{s + z_c}{s + p_c}$	<ol style="list-style-type: none"> <li>Error is improved but not driven to zero.</li> <li>Pole at <math>-p_c</math> is small and negative.</li> <li>Zero at <math>-z_c</math> is close to, and to the left of, the pole at <math>-p_c</math>.</li> <li>Active circuits are not required to implement.</li> </ol>
Improve transient response	PD	$K(s + z_c)$	<ol style="list-style-type: none"> <li>Zero at <math>-z_c</math> is selected to put design point on root locus.</li> <li>Active circuits are required to implement.</li> <li>Can cause noise and saturation; implement with rate feedback or with a pole (lead).</li> </ol>
Improve transient response	Lead	$K \frac{s + z_c}{s + p_c}$	<ol style="list-style-type: none"> <li>Zero at <math>-z_c</math> and pole at <math>-p_c</math> are selected to put design point on root locus.</li> <li>Pole at <math>-p_c</math> is more negative than zero at <math>-z_c</math>.</li> <li>Active circuits are not required to implement.</li> </ol>
Improve steady-state error and transient response	PID	$K \frac{(s + z_{lag})(s + z_{lead})}{s}$	<ol style="list-style-type: none"> <li>Lag zero at <math>-z_{lag}</math> and pole at origin improve steady-state error.</li> <li>Lead zero at <math>-z_{lead}</math> improves transient response.</li> <li>Lag zero at <math>-z_{lag}</math> is close to, and to the left of, the origin.</li> <li>Lead zero at <math>-z_{lead}</math> is selected to put design point on root locus.</li> <li>Active circuits required to implement.</li> <li>Can cause noise and saturation; implement with rate feedback or with an additional pole.</li> </ol>
Improve steady-state error and transient response	Lag-lead	$K \frac{(s + z_{lag})(s + z_{lead})}{(s + p_{lag})(s + p_{lead})}$	<ol style="list-style-type: none"> <li>Lag pole at <math>-p_{lag}</math> and lag zero at <math>-z_{lag}</math> are used to improve steady-state error.</li> <li>Lead pole at <math>-p_{lead}</math> and lead zero at <math>-z_{lead}</math> are used to improve transient response.</li> <li>Lag pole at <math>-p_{lag}</math> is small and negative.</li> <li>Lag zero at <math>-z_{lag}</math> is close to, and to the left of, lag pole at <math>-p_{lag}</math>.</li> <li>Lead zero at <math>-z_{lead}</math> and lead pole at <math>-p_{lead}</math> are selected to put design point on root locus.</li> <li>Lead pole at <math>-p_{lead}</math> is more negative than lead zero at <math>-z_{lead}</math>.</li> <li>Active circuits are not required to implement.</li> </ol>

### Lag Compensator



Lag compensation improves steady-state error in unity feedback system

Lag compensation techniques based on the frequency response approach

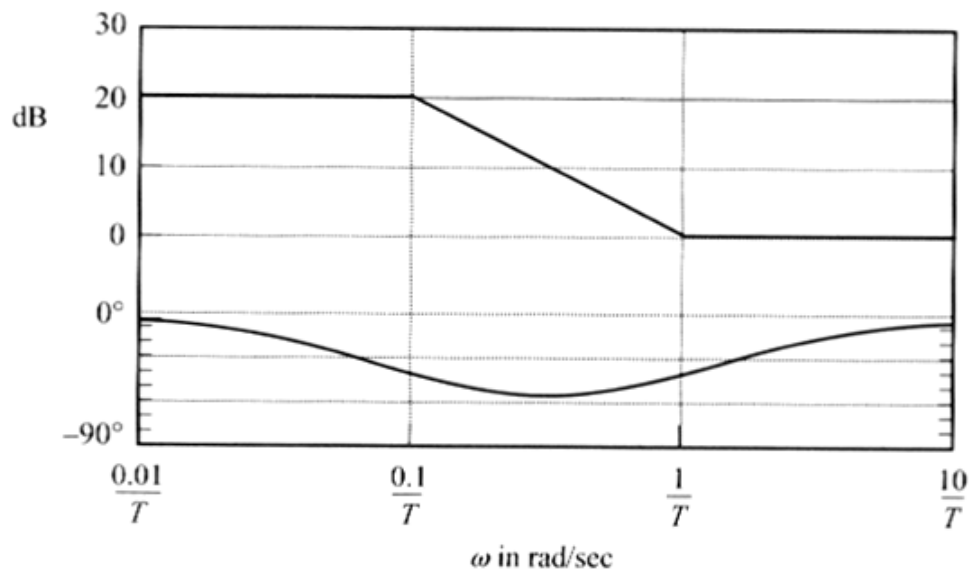
Lag compensator transfer function

$$G_c(s) = K_c \beta \frac{Ts + 1}{\beta Ts + 1} = K_c \frac{s + \frac{1}{T}}{s + \frac{1}{\beta T}} \quad (\beta > 1)$$

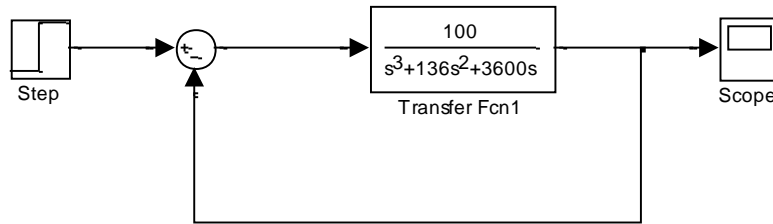
Zero of lag compensation is  $\frac{1}{T}$

Pole of lag compensation is  $\frac{1}{\beta T}$

Compensate magnitude and phase profile shown in figure



**Example** Lag design ; Desired system is  $K_v$  of  $16.22 \text{ sec}^{-1}$ , PM of 60 degree and GM of least 10 dB



Determine and analysis of previous information

Open-loop TF is

; Type \_\_\_\_\_

Closed-loop TF is

Closed-loop poles are \_\_\_\_\_

Bandwidth frequency ( $\omega_{BW}$ ) = \_\_\_\_\_ rad/sec

Gain margin(GM) = \_\_\_\_\_ dB; Phase margin(PM) = \_\_\_\_\_ degree

Static velocity error constant ( $K_v$ ) = \_\_\_\_\_  $\text{sec}^{-1}$

Settling time = \_\_\_\_\_ sec (5% error)

**Step I:** Determine total gain ( K ) of open-loop TF to satisfy the requirement on the given static velocity error constant (  $K_v$  )= 16.22

$$K_v = \lim_{s \rightarrow 0} sG_c(s)G(s) = \lim_{s \rightarrow 0} s \left( K_c \beta \frac{Ts + 1}{\beta Ts + 1} \right) \left( \frac{100}{s(s + 36)(s + 100)} \right) = 16.22$$

where  $K_c \beta = K$ , thus

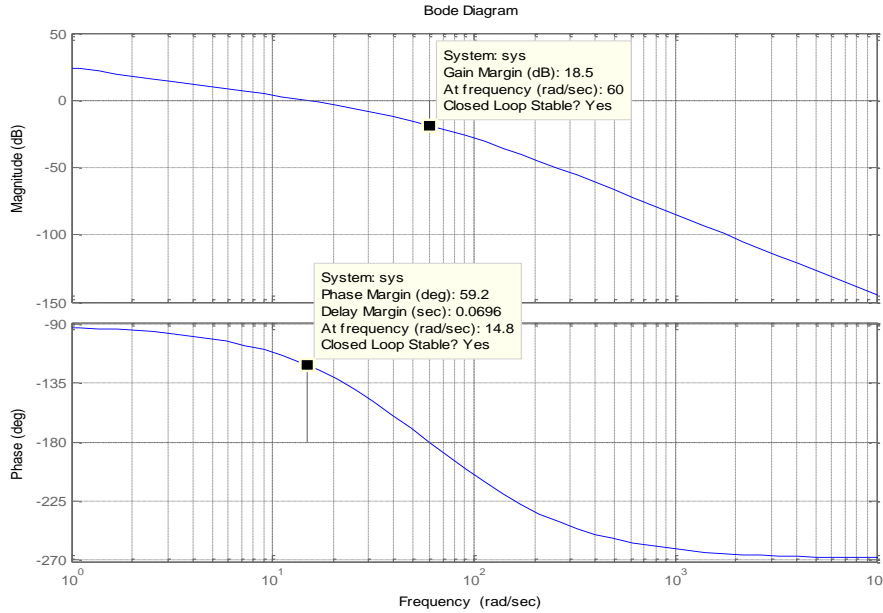
$$K = 16.22(36) = 583.92$$

New open-loop transfer function

$$G_0(s) = \frac{16.22(36)}{(s+100)(s+36)s} = \frac{58392}{s^3 + 136s^2 + 3600s}$$

**Step II:** Plot bode diagram of new open-loop TF with new gain such as

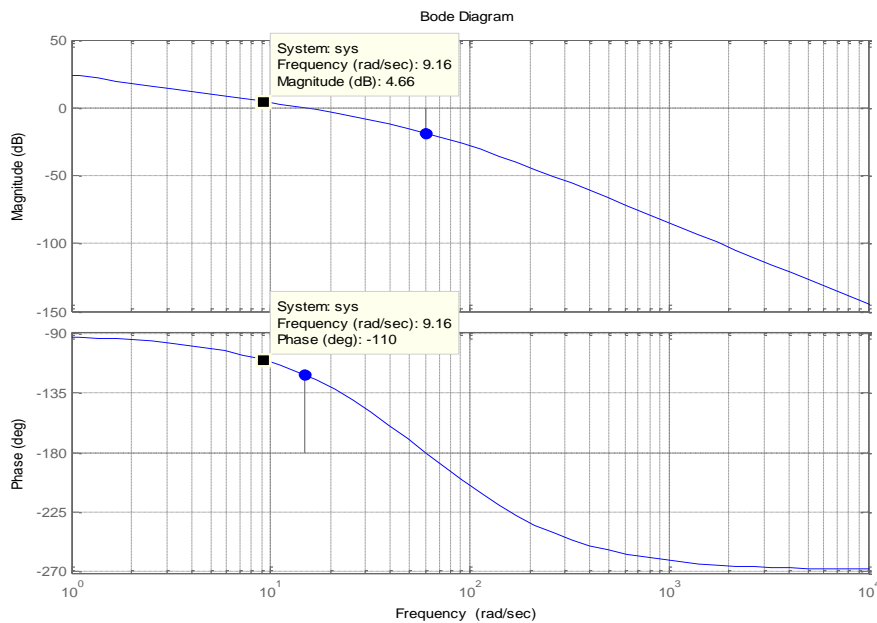
$$G_0(s) = \frac{58392}{(s+100)(s+36)s} = \frac{58392}{s^3+136s^2+3600s}$$



**Determine:** Phase margin(PM)= 59.2 deg. at 14.8 rad/sec ; Gain margin(GM)= 18.5 dB at 60 rad/sec

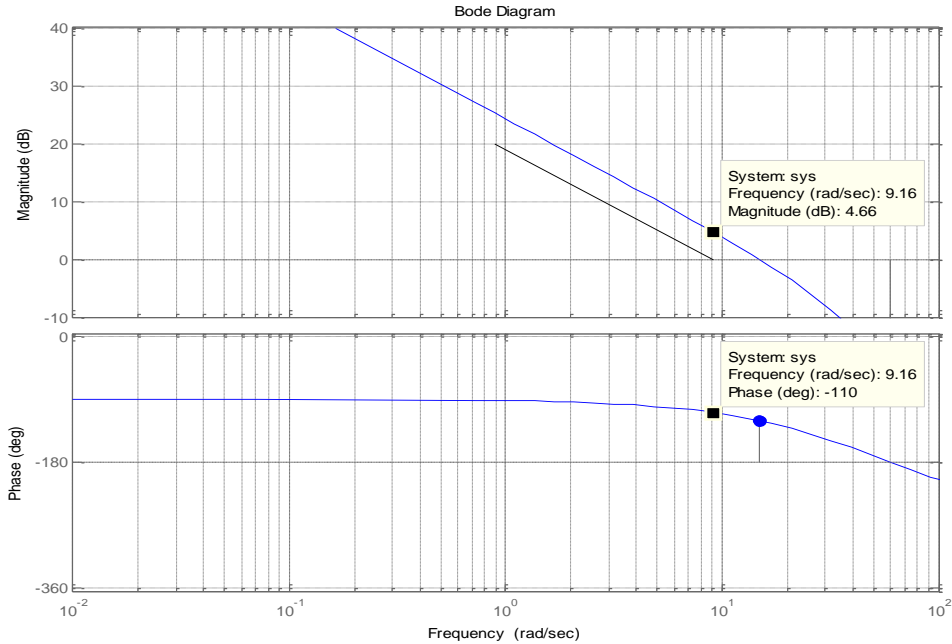
**Step III:** Phase margin requirement is 60 deg. plus 10 deg. Total PM requirement is 60+10 = 70 deg.

For PM of 70 deg., -180+70 = - 110 deg. ; At 9.16 rad/sec has phase -110 deg. and magnitude is 4.66 dB. We must change phase margin frequency from 14.8 rad/sec to 9.16 rad/sec



**Step IV:** The corner frequency  $\omega = 1/T$  may be chosen 1 decade below the new gain crossover frequency

At 0.916 rad/sec is zero of lag compensation such as  $\frac{1}{T} = 0.916 \rightarrow T = 1.092$



**Step V:**  $20 \log \frac{1}{\beta} = -4.66 \rightarrow \beta = 1.71$

Pole of lag compensation is  $\frac{1}{\beta T} = 0.5357$

Now lag compensator is  $G_c(s) = K_c \frac{s+0.916}{s+0.5357}$

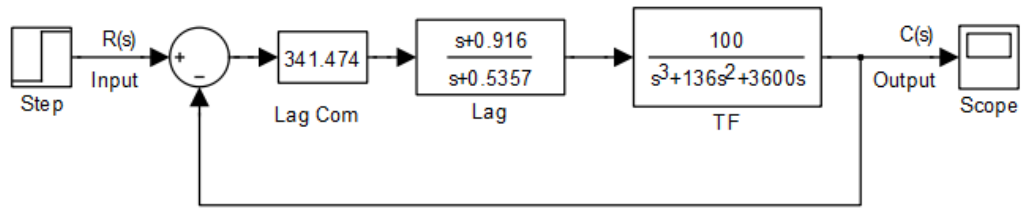
**Step VI:** Determine gain of lag compensator

$$G_c(s) = K_c \frac{s + 1/T}{s + 1/\beta T} = K_c \frac{s + 0.916}{s + 0.5357}$$

$$T = \frac{1}{0.916} = 1.092; \beta = 1.71;$$

$$K_c \beta = K = 583.92 \rightarrow K_c = 341.474$$

Now lag compensator is  $G_c(s) = 341.474 \left( \frac{s+0.916}{s+0.5357} \right)$



Check steady state error for unit-ramp input relation with velocity constant and PM relation with damping ratio (% overshoot)

